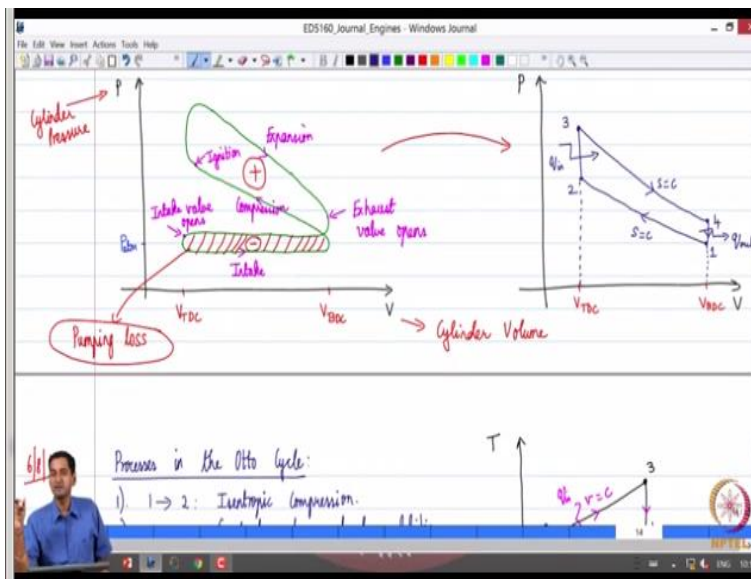


**Fundamentals of Automotive Systems**  
**Prof. C.S. Shankar Ram**  
**Department of Engineering Design**  
**Indian Institute of Technology-Madras**

**Lecture-09**  
**Otto Cycle and Diesel Cycle**  
**Part 01**

(Refer Slide Time: 00:15)

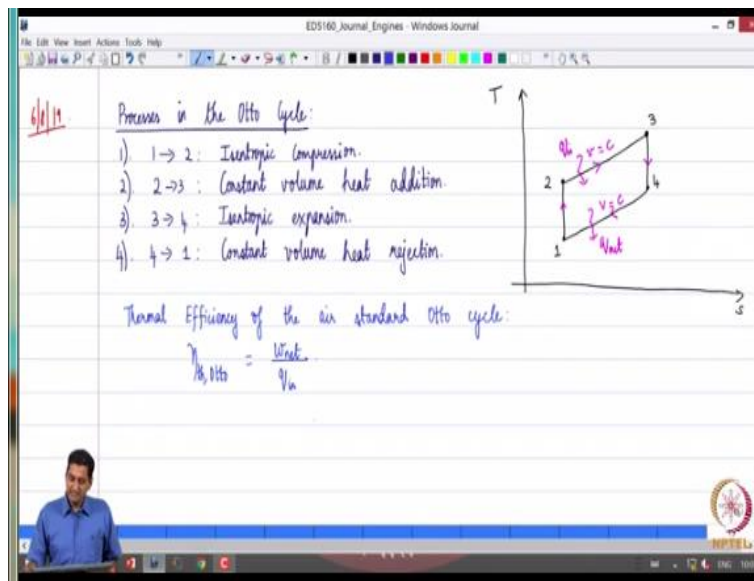


Okay greetings, welcome to today's class, so we were looking at the otto cycle yesterday. So just a quick recap we were looking at what are called as air standard cycles which are typically used to do a first cut analysis of IC engine performance and we saw what was an air standard cycle, what were the assumptions typically mean and we started off with the otto cycle right and just to quickly recap what we discussed looking at the PV diagram of this otto cycle.

So we map the various processes of intake compression power stroke and the exhaust stroke which are quickly found in a 4 stroke IC engine and we observed that it was mapped to a simpler version which where the so called pumping losses were not considered. So as far as the otto cycle is concerned we consider an equivalent piston and cylinder assembly in which the working fluid is just higher and we start from the compression process ok.

We do not consider the intake and the exhaust processes as such we only consider the compression process it should be 1 to 2 then the combustion process is replaced by a heat addition process that takes place at constant volume. Then there is an expansion process from 3 to 4 which is once again assumed to be isentropic and 4 to 1 is a constant volume heat rejection process and the motivation for this approximation comes from the shape of the PV diagram which is typically observed when we do measurements from an gasoline or a petrol engine ok.

**(Refer Slide Time: 02:22)**



So that is the motivation here, so just to list all the strokes all the what to say processes in an otto cycle or I should say in the otto cycle the process from 1 to 2 is isentropic compression ok. The process from 2 to 3 is constant volume heat addition, the process from 3 to 4 is isentropic expansion, the process from 4 to 1 is constant volume heat rejection. So these are the 4 processes right that are involved in this air standard otto cycle.

So some people will call this as the air standard otto cycle some could referred to as just otto cycle and so on right ok. So now if we were to draw the Ts diagram for the same cycle ok we will shortly see that sometimes the Ts diagram is also pretty useful in analyzing these processes T stands for temperature, s stands for entropy ok. So if we were to map the same 4 processes let us say we start with state 1, 1 to 2 will be isentropic compressions.

So in the  $Ts$  plot it is going to go vertically upwards right, so that is going to be isentropic compression and 2 to 3 is constant volume heat addition. So it is going to go something like this 3 to 4 is isentropic expansion, so that is going to go curve something like this and then fourth one is constant volume heat rejection ok. So if I were to mark all the processes it is important to mark important characteristics of each process and also the direction of the entire cycle right.

So this will be  $V$  is equal to constant ok, so this is the process where heat is added and this is the process where heat is released ok. So these are the 4 processes of the same air standard otto cycle expressed in the  $Ts$  plane ok. So now if I were to obtain an expression for the thermal efficiency of the air standard otto cycle you can immediately see that the thermal efficiency for the air standard otto cycle is going to be the net work done divided by the net heat which is input right.

So efficiency is like output by input this case the output is the network output of the otto cycle. The input is the heat input which we given right, so how do we get expressions for these right.

**(Refer Slide Time: 06:17)**

Recall that the first law of thermodynamics can be expressed as

$$dq - dw = de, \quad e = u + ke + pe$$

When integrated over a cycle,

$$\oint dq - \oint dw = \oint de = 0 \quad \Rightarrow \quad q_{in} = w_{net} \rightarrow \text{for a cycle.}$$

$$\Rightarrow \quad w_{net} = q_{in} - q_{out}$$

$$\Rightarrow \quad \eta_{otto} = \frac{w_{net}}{q_{in}} = \frac{q_{in} - q_{out}}{q_{in}} = 1 - \frac{q_{out}}{q_{in}}$$

So recall that the first law of thermodynamics can be expressed as in differential form right, so it can be expressed as  $\delta q - \delta w = de$  where the net energy  $e$  is a sum of the internal energy + the kinetic energy + the potential energy right. So this is a standard form for the first law of thermodynamics that people will use ok when integrated over a cycle what is going to happen, it going to get  $\delta q - \delta w = \int \text{over the cycle } de$  right.

So kindly recall from thermodynamics that heat transfer and work interactions are all path dependent quantities right, whereas the net energy is a path independent quantity right. So if I integrate over a cycle what is going to happen to this integral over a cycle of  $de$ , this is going to become 0 right because we end up at the same initial state right. So essentially since it is a path independent quantity it only depends on the final state and the initial state.

And since the 2 states happen to be the same, the net change is going to be 0, so the net heat transfer is going to be equal to the network output for a cycle ok, this expression is true when you have a cycle right. So the net heat transfer over a cycle is going to be equal to the net work output from that cycle, so what can we say about this otto cycle the network output of the Otto cycle should be equal to the net heat input given to the otto cycle.

The net heat input is going to be the heat which is given in minus the heat which is taken out or rejected right that is going to be  $q_{in} - q_{out}$ . So going back this would give me  $\eta_{thermal}$  for the otto cycle will be equal to  $w_{net}$  by  $q_{in}$  that is going to be equal to  $q_{in} - q_{out}$  divided by  $q_{in}$  in which I can rewrite as  $1 - q_{out} / q_{in}$  ok very standard expression. So now what about the expressions for  $q_{out}$  and  $q_{in}$  alright. So that is the next analysis that we need to do, so if we recall the heat addition takes place at constant volume right.

**(Refer Slide Time: 09:30)**

EDS160\_Journal\_Engines - Windows Journal

Heat rejection, 4 to 1:  $\int_4^1 T dv = \int_4^1 p dv = \int_4^1 de = u_1 - u_4$  (neglecting changes in ke & pe)

Heat addition, 2 to 3:  $\int_2^3 T dv = \int_2^3 p dv = \int_2^3 de = u_3 - u_2$

$W_{net} = Q_{in} - Q_{out}$

$\Rightarrow \eta_{th, Otto} = \frac{W_{net}}{Q_{in}} = \frac{Q_{in} - Q_{out}}{Q_{in}} = 1 - \frac{Q_{out}}{Q_{in}}$

$\Rightarrow Q_{in} = u_3 - u_2$

Heat rejection, 4 to 1:  $\int_4^1 T dv = \int_4^1 p dv = \int_4^1 de \Rightarrow Q_{out} = u_1 - u_4$

$\Rightarrow Q_{out} = u_1 - u_4$

$\Rightarrow \eta_{th, Otto} = 1 - \frac{Q_{out}}{Q_{in}} = 1 - \frac{(u_1 - u_4)}{(u_3 - u_2)}$

NPTEL

So the heat addition process is the process from 2 to 3 right that is the one which takes place at constant volume right. So if we integrate the first law of thermodynamics over the process 2 to 3 what are we going to get, so this is going to be  $q_{in}$ , this is going to be equal to 0 because the heat addition process takes place at constant volume ok. Then this I can write it as  $u_3 - u_2$  neglecting changes in kinetic energy and potential energy which is a reasonable assumption here right.

So considering the system and the process that it undergoes I can neglect the changes in kinetic and potential. So this implies that my heat input  $q_{in}$  is going to be equal to  $u_3 - u_2$  right, so that is 1, similarly I can consider the heat rejection process that is from 4 to 1. So doing the same analysis from 4 to 1 ok  $dq_{4 \rightarrow 1} = \delta w_{4 \rightarrow 1} + du_{4 \rightarrow 1}$  we are going to get  $q_{out}$  to be equal to  $u_1 - u_4$ . Of course here you know like the if I have to be very careful I should have written this has the absolute value of  $q_{out}$  ok going back right.

So because  $q_{out}$  is a heat rejected from the otto cycle right, so any the sign convention in thermodynamics is that like if heat is taken from the system it is sign is negative ok and if heat is given to a system the sign of that quantity is going to be positive ok. So that is the sign convention that we utilize right, so I will use the  $q_{out}$  instead of that I will use absolute magnitude of  $q_{out}$  ok here even here ok.

So you can immediately see that this  $q_{out}$  is going to be negative because you  $N$  is going to be less than  $u_4$ , so this implies the absolute value of  $q_{out}$  it is going to be equal to  $u_4 - u_1$  ok. So I am just rewriting, so that we are consistent ok, so now we are all set to look at the thermal efficiency expression once again. So we can immediately see that the thermal efficiency of the air standard Otto cycle is  $1 - \text{magnitude of } q_{out} \text{ by } q_{in}$ . This is going to be  $1 - u_4 - u_1$  divided by  $u_3 - u_2$  and assuming constant specific heats.

**(Refer Slide Time: 12:57)**

The image shows a handwritten derivation of the thermal efficiency of an Otto cycle in a Windows Journal window. The derivation is as follows:

$$\Rightarrow \eta_{th, Otto} = 1 - \frac{|q_{out}|}{q_{in}} = 1 - \frac{(u_4 - u_1)}{(u_3 - u_2)} = 1 - \frac{C_v(T_4 - T_1)}{C_v(T_3 - T_2)}$$

*(constant specific heats)*

Isentropic compression, 1 → 2:  $T_1 V_1^{(\gamma-1)} = T_2 V_2^{(\gamma-1)} \Rightarrow T_2 = T_1 \left( \frac{V_1}{V_2} \right)^{(\gamma-1)} = T_1 \lambda^{(\gamma-1)}$   
 $\gamma = \frac{C_p}{C_v}$

Isentropic expansion, 3 → 4:  $T_3 V_3^{(\gamma-1)} = T_4 V_4^{(\gamma-1)} \Rightarrow T_4 = T_3 \left( \frac{V_3}{V_4} \right)^{(\gamma-1)} = T_3 \lambda^{(\gamma-1)}$

$$\Rightarrow \eta_{th, Otto} = 1 - \frac{(T_4 - T_1)}{T_3 \lambda^{(\gamma-1)} - T_1 \lambda^{(\gamma-1)}} \Rightarrow \eta_{th, Otto} = 1 - \frac{1}{\lambda^{(\gamma-1)}}$$

We know from thermodynamics then delta u is going to be C v times delta T right, so we make the assumption of constant specific heats. So this is going to be 1 – C v T 4 - T1 divided by C v T 3 – T 2, so C v and C v cancel ok, so we are not it done right we need to simplify it further. Now **we** what we have done we have essentially reduce the expression for the thermal efficiency of the Otto cycle in terms of temperatures at the critical states right the 4 corner states if I can call them that right or the nodes are 1 and 2, 1 2 3 and 4 right.

So we have reduce the expression in terms of temperatures now let us go further right. Let us use the other 2 processes right, so till now we have used processes 2 to 3 and 4 to 1 what about the other 2 processes right. So let us look at the isentropic compression process, isentropic compression process is the process from 1 to 2, so the process relationship is going to be typically the isentropic process is basically governed by P v power gamma equals constant that is how we write down what is called as a process relationship right for an isentropic process.

So using the ideal gas equation of state along with that we can always rewrite that as T V power gamma - 1 = constant, so I can write T 1 V 1 power gamma - 1 = T 2 V 2 power gamma - 1 ok. So this is what is called as a process relationship ok, so this governs the isentropic process. So this will give me T 2 = T 1 V 1 by V 2 to the power gamma - 1, so by the way what is gamma is nothing but the ratio of specific heats C p by C v right.

So typically its value is taken as 1.44 for air under standard conditions right, so that is the meaning of gamma. So now if we look at this  $T_2$  is  $T_1 V_1^{1/\gamma} T_1^{1-\gamma} V_2^{1/\gamma}$  but what is  $V_1/V_2$ , if we go up  $V_1$  is the volume and bottom dead center,  $V_2$  is the volume and top dead center. So what is the ratio called as compression ratio right, so that is the definition of compression ratio.

So immediately we can see that  $T_2$  is going to be equal to  $T_1 r^{1/\gamma}$  where  $r$  is nothing but  $V_1/V_2$  ok, so this is the compression ratio  $r$  ok. So similarly let us consider the isentropic expansion process which is from 3 to 4, so what happens here, so the process relationship becomes this. So this will give me  $T_4$  or I can say  $T_3 = T_4 V_4^{1/\gamma} V_3^{1-\gamma}$  to the power gamma - 1.

So once again what is  $V_4/V_3$ ,  $V_4$  is here volume at BDC  $V_3$  is also volume at TDC right because the heat addition and rejection process both take place at constant volume. So what is going to be  $V_4/V_3$  once again  $r$  the compression ratio right, so this implies the  $T_3$  is going to be equal to  $T_4 r^{1/\gamma}$  ok we are almost done now. So substituting these we immediately get the thermal efficiency of the air standard Otto cycle to be  $1 - T_4/T_3$  divided by  $T_3$  I am going to substitute  $T_4 r^{1/\gamma}$  to the power gamma - 1.

For  $T_2$  let us substitute  $T_1 r^{1/\gamma}$  to the power gamma - 1, so if you simplify this what is it that we will get we can immediately see that  $r^{1/\gamma}$  to the power gamma - 1 is common in the denominator if you take it out you get  $T_4 - T_1$  and that factor cancels between the numerator and the denominator. So the thermal efficiency of the air standard Otto cycle reduces to  $1 - 1/r^{1/\gamma}$  divided by  $r^{1/\gamma}$  to the power gamma - 1, so you see that it reduces to a very simple expression ok.

So the thermal efficiency of the Otto cycle depends only on air standard Otto cycle right depends only on the compression ratio  $r$ .

**(Refer Slide Time: 19:05)**

$$T_1 V_1^{(\gamma-1)} = T_2 V_2^{(\gamma-1)} \Rightarrow T_2 = T_1 \left( \frac{V_1}{V_2} \right)^{(\gamma-1)} = T_1 r^{(\gamma-1)}$$

$$T_3 V_3^{(\gamma-1)} = T_4 V_4^{(\gamma-1)} \Rightarrow T_3 = T_4 \left( \frac{V_4}{V_3} \right)^{(\gamma-1)} = T_4 r^{(\gamma-1)}$$

$$\Rightarrow \eta_{th, Otto} = 1 - \frac{(T_4 - T_1)}{T_4 r^{(\gamma-1)} - T_1 r^{(\gamma-1)}} \Rightarrow \eta_{th, Otto} = 1 - \frac{1}{r^{(\gamma-1)}}$$

As  $r \uparrow$ ,  $\eta_{th, Otto} \uparrow$ . However, the phenomenon of knocking in SI engines limits the value of  $r$ .

So we can immediately observe that as the compression ratio increases the value of the thermal efficiency also increases right. Because you can immediately see that as  $r$  increases  $r^{\gamma-1}$  will increase it is reciprocal will decrease and we are subtracting a smaller number from 1 right. So the thermal efficiency will increase right but however we will later study what is called as the phenomenon of knocking in SI engines and this limits the value of  $r$  ok.

So we can keep on increasing the value of compression ratio ok there is something called knocking in SI engines which restricts the value of  $r$  ok we will look at that later ok when we come to the analysis of the combustion process in assignments ok. So to quickly summarize in the air standard Otto cycle we looked at the 4 processes the main feature is that like the heat addition process is assumed to take place at constant volume in the Otto cycle.

We use simple expressions that we learnt in thermodynamics right to derive an expression for the thermal efficiency ok, so that is what we have done ok.